## 100608 Final Exam Materials and Energy Balances

 ANSWERS ON SEPARATE SHEETS. NAME IN THE UPPER RIGHT CORNER OF EACHPAGE AND NUMBER THE PAGES. (LEAVE (TOP LEFT) ROOM FOR A STAPLE)
(Gas constant, g, Cox chart, Tables B1, B2, B5, B6, B8, B9, and periodic table at the end.)
1)* A mixture of methane and air can be ignited at mole percentages of methane between $5 \%$ and $15 \%$.
a) Why might this the case, i.e. what happens at lower or higher concentrations?
b) For a mixture of 9.0 mole $\%$ methane at flow rate of $700 . \mathrm{kg} / \mathrm{h}$ needs to be diluted below the flammability limit. Calculate the required flow rate of air in mole $/ \mathrm{h}$.
c) Calculate the concentration of oxygen in percent by mass in the product gas.
*Modified from Question 3.23 of the R.M. Felder and R.W. Rousseau Text.
2)* When a fireplace is used, a draft is induced that causes the hot gases to flow up the stack. The theoretical draft, $\mathrm{D}\left(\mathrm{N} / \mathrm{m}^{2}\right)$ is the difference in the hydrostatic head in the stack and ant the furnace inlet. The actual draft takes in to account pressure losses in the flowing gasses. Let $T_{s}(K)$ be the average temperature in a stack of height $L(m)$ and $T_{a}$ the ambient temperature and let $M_{s}$ and $M_{a}$ be the average molecular weights of the gases inside and outside the stack. Assume that the pressures inside and outside the stack are both equal to atmospheric pressure, $\mathrm{P}_{\mathrm{a}}\left(\mathrm{N} / \mathrm{m}^{2}\right)$.
a) Use the ideal gas law to obtain an expression for the theoretical draft as a function of $P_{a}, L, g, R, M_{a}, T_{a}, M_{s}$ and $T_{s}$.
b) Describe 3 other methods/equations, discussed in class, that could be used to give a better expression for the theoretical draft.
c) Suppose the gas in a $53-\mathrm{m}$ stack has an average temperature of $655^{\circ} \mathrm{K}$ and contains 18 mole $\% \mathrm{CO}_{2}, 2 \% \mathrm{O}_{2}$, and $80 \% \mathrm{~N}_{2}$ with barometric pressure of 755 mm Hg and outside temperature $294^{\circ} \mathrm{K}$. Calculate the theoretical draft ( mm Hg ) induced in the furnace.
d) How could the draft be improved?
*Modified from Question 5.28 of the R.M. Felder and R.W. Rousseau Text.
3)* Saturated steam at a gauge pressure of 2.0 bar is to be used to heat a stream of ethane. The ethane enters a heat exchanger at $16^{\circ} \mathrm{C}$ and 1.5 bar gauge at a rate of $795 \mathrm{~m}^{3} / \mathrm{min}$ and is heated at constant pressure to $93^{\circ} \mathrm{C}$. The steam condenses and leaves the exchanger as a liquid at $27^{\circ} \mathrm{C}$. The specific enthalpy of ethane at the given pressure is $941 \mathrm{~kJ} / \mathrm{kg}$ at $16^{\circ} \mathrm{C}$ and $1073 \mathrm{~kJ} / \mathrm{kg}$ at $93^{\circ} \mathrm{C}$.
a) Draw a flow diagram and do a degree of freedom analysis for this problem.
b) How much energy ( kW ) must be transferred to the ethane to heat it from $16^{\circ} \mathrm{C}$ to $93^{\circ} \mathrm{C}$ ? (Write the energy balance and list all assumptions.)
c) Assuming that all the energy transferred from the steam goes to heat the ethane, at what rate in $\mathrm{m}^{3} / \mathrm{s}$ must steam be supplied to the exchanger? If the assumption is incorrect, would the calculated value be too high or too low?
d) Should the heat exchanger be set up for co-current or counter-current flow? Explain.
*Modified from Question 7.28 of the R.M. Felder and R.W. Rousseau Text.
4)*

Hydrogen is produced in the steam reforming of propane:

$$
\mathrm{C}_{3} \mathrm{H}_{8}(\mathrm{~g})+3 \mathrm{H}_{2} \mathrm{O}(\mathrm{v}) \rightarrow 3 \mathrm{CO}(\mathrm{~g})+7 \mathrm{H}_{2}(\mathrm{~g})
$$

The water-gas shift reaction also takes place in the reactor, leading to the formation of additional hydrogen:

$$
\mathrm{CO}(\mathrm{~g})+\mathrm{H}_{2} \mathrm{O}(\mathrm{v}) \rightarrow \mathrm{CO}_{2}(\mathrm{~g})+\mathrm{H}_{2}(\mathrm{~g})
$$

The reaction is carried out over a nickel catalyst in the tubes of a shell-and-tube reactor. The feed to the reactor contains steam and propane in a $6: 1$ molar ratio at $125^{\circ} \mathrm{C}$, and the products emerge at $800^{\circ} \mathrm{C}$. The excess steam in the feed assures essentially complete consumption of the propane. Heat is added to the reaction mixture by passing a hot gas over the outside of the tubes that contain the catalyst. The gas is fed at $4.94 \mathrm{~m}^{3} / \mathrm{mol} \mathrm{C}_{3} \mathrm{H}_{8}$, entering the unit at $1400^{\circ} \mathrm{C}$ and 1 atm and leaving at $900^{\circ} \mathrm{C}$. The unit may be considered adiabatic.


Calculate the molar composition of the product gas, assuming that the heat capacity of the heating gas is $0.040 \mathrm{~kJ} /\left(\mathrm{mol}^{\circ}{ }^{\circ} \mathrm{C}\right)$.
*Question 9.37 of the R.M. Felder and R.W. Rousseau Text.

## PERIODIC TABLE OF THE ELEMENTS



## THE GAS CONSTANT

| $8.314 \mathrm{~m} \cdot \mathrm{~Pa} /(\mathrm{mol} \cdot \mathrm{K})$ |
| :---: |
| $0.08314 \mathrm{~L} \cdot \mathrm{bar} /(\mathrm{mol} \cdot \mathrm{K})$ |
| $0.08206 \mathrm{~L} \cdot \mathrm{~atm} /(\mathrm{mol} \cdot \mathrm{K})$ |
| $62.36 \mathrm{~L} \cdot \mathrm{~mm} \mathrm{Hg} /(\mathrm{mol} \cdot \mathrm{K})$ |
| $0.7302 \mathrm{ft} \cdot \mathrm{atm} /\left(\mathrm{lb}-\mathrm{mole} \cdot{ }^{\circ} \mathrm{R}\right)$ |
| $10.73 \mathrm{ft}^{3} \cdot \mathrm{psia} /\left(\mathrm{lb}-\mathrm{mole} \cdot{ }^{\circ} \mathrm{R}\right)$ |
| $8.314 \mathrm{~J} /(\mathrm{mol} \cdot \mathrm{K})$ |
| $1.987 \mathrm{cal} /(\mathrm{mol} \cdot \mathrm{K})$ |
| $1.987 \mathrm{Btu} /\left(\mathrm{lb}-\mathrm{mole} \cdot \cdot{ }^{\circ} \mathrm{R}\right)$ |


| Table B.1 Selected $\mathrm{Physical} \mathrm{Property} \mathrm{Data}^{a}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |

Table B. 1 (Continued)

| Compound | Formula | Mol. Wt. | $\begin{gathered} \text { SG } \\ \left(20^{\circ} / 4^{\circ}\right) \end{gathered}$ | $T_{\mathrm{m}}\left({ }^{\circ} \mathrm{C}\right)^{b}$ | $\begin{gathered} \Delta \hat{H}_{\mathrm{m}}\left(T_{\mathrm{m}}\right)^{\mathrm{c},} \\ \mathrm{~kJ} / \mathrm{mol} \end{gathered}$ | $T_{\mathrm{b}}\left({ }^{\circ} \mathrm{C}\right)^{d}$ | $\Delta \hat{H}_{\mathrm{v}}\left(T_{\mathrm{b}}\right)^{\mathrm{c}}$ <br> $\mathrm{kJ} / \mathrm{mol}$ | $T_{\mathrm{c}}(\mathrm{K})^{f}$ | $P_{\text {c }}(\mathrm{atm})^{g}$ | $\left(\Delta \hat{H}_{\mathrm{f}}{ }^{\circ}\right)^{h, j}$ <br> $\mathrm{kJ} / \mathrm{mol}$ | $\left(\Delta \hat{H}_{\mathrm{c}}{ }^{\circ}\right)^{i, j}$ <br> $\mathrm{kJ} / \mathrm{mol}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Chloroform | $\mathrm{CHCl}_{3}$ | 119.39 | 1.489 | -63.7 | - | 61.0 |  | 536.0 | 54.0 | -131.8(1) | -373(1) |
| Copper | Cu | 63.54 | 8.92 | 1083 | 13.01 | 2595 | 304.6 | - |  | 0(c) |  |
| Cupric sulfate | $\mathrm{CuSO}_{4}$ | 159.61 | $3.606^{15^{\circ}}$ | Decomposes $>600^{\circ} \mathrm{C}$ |  |  |  |  |  | $\begin{aligned} & -769.9(\mathrm{c}) \\ & -843.1(\mathrm{aq}) \end{aligned}$ | - |
| Cyclohexane | $\mathrm{C}_{6} \mathrm{H}_{12}$ | 84.16 | 0.779 | 6.7 | 2.677 | 80.7 | 30.1 | 553.7 | 40.4 | -843.1(aq) | -3919.9(l) |
| Cyclopentane | $\mathrm{C}_{5} \mathrm{H}_{10}$ | 70.13 | 0.745 | -93.4 | 0.609 | 49.3 | 27.30 | 511 | 44. | -123.1(g) | -3953.0(g) |
|  |  |  |  |  |  |  |  |  |  | -77.2(g) | -3290.9(1) |
| $n$-Decane | $\mathrm{C}_{10} \mathrm{H}_{22}$ | 142.28 | 0.730 | -29.9 | - | 173.8 | - | 619.0 | 20.8 | -249.7(1) | -6778.3(1) |
| Diethyl ether | $\left(\mathrm{C}_{2} \mathrm{H}_{5}\right)_{2} \mathrm{O}$ | 74.12 | $0.708^{25^{\circ}}$ | -116.3 | 7.30 | 34.6 | 26.05 | 467 | 35.6 | -272.8(1) | -6829.7(g) |
| Ethane | $\mathrm{C}_{2} \mathrm{H}_{6}$ | 30.07 | - | -183.3 | 2.859 | -88.6 | 14.72 | 305.4 | 35.6 48.2 | $\begin{aligned} & -272.8(1) \\ & -84.67(\mathrm{~g}) \end{aligned}$ | $\begin{aligned} & -2726.7(\mathrm{I}) \\ & -1559.9(\mathrm{~g}) \end{aligned}$ |
| Ethyl acetate | $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{2}$ | 88.10 | 0.901 | -83.8 | - | 77.0 | - | 523.1 | 37.8 | -463.2(1) | $-2246.4(1)$ |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Ethyl alcohol (Ethanol) | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | 46.07 | 0.789 | -114.6 | 5.021 | 78.5 | 38.58 | 516.3 | 63.0 | $\begin{aligned} & -277.63(\mathrm{l}) \\ & -235.31(\mathrm{~g}) \end{aligned}$ | $\begin{aligned} & -1366.91(\mathrm{l}) \\ & -1409.25(\mathrm{~g}) \end{aligned}$ |
| Ethyl benzene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | 106.16 | 0.867 | -94.67 | 9.163 | 136.2 | 35.98 | 619.7 | 37.0 | -12.46(1) | -4564.9(1) |
| Ethyl bromide | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | 108.98 | 1.460 | -119.1 | - | 38.2 | - | 50 |  | +29.79(g) | -4607.1(g) |
| Ethyl chloride | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ | 64.52 | $0.903^{15^{\circ}}$ | -138.3 | 4.452 | 13.1 | 24.7 | 460.4 | 52.0 | $-54.4(\mathrm{~g})$ $-105.0(\mathrm{~g})$ | - |
| 3-Ethyl hexane | $\mathrm{C}_{8} \mathrm{H}_{18}$ | 114.22 | 0.717 | - | - | 118.5 | 34.27 | 567.0 | 26.4 | $\begin{aligned} & -250.5(\mathrm{l}) \\ & -210.9(\mathrm{~g}) \end{aligned}$ | $\begin{aligned} & -5407.1(\mathrm{l}) \\ & -5509.8(\mathrm{~g}) \end{aligned}$ |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4}$ | 28.05 | - | -169.2 | 3.350 | -103.7 | 13.54 | 283.1 | 50.5 | +52.28(g) | $\begin{aligned} & -5509.8(\mathrm{~g}) \\ & -1410.99(\mathrm{~g}) \end{aligned}$ |
| Ethylene glycol | $\mathrm{C}_{2} \mathrm{H}_{6} \mathrm{O}_{2}$ | 62.07 | $1.113^{19^{\circ}}$ | -13 | 11.23 | 197.2 | 56.9 | - | - | $\begin{aligned} & -451.5(1) \\ & -387.1(\mathrm{~g}) \end{aligned}$ | -1179.5(1) |
| Ferric oxide | $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | 159.70 | 5.12 |  |  |  |  |  |  | -822.2(c) |  |
| Ferrous oxide | FeO | 71.85 | 5.7 | - | - | - | - | - | - | -266.5(c) | - |
| Ferrous sulfide | FeS | 87.92 | 4.84 | 1193 | - | - | - | - | - | -95.1(c) | - |
| Formaldehyde | $\mathrm{H}_{2} \mathrm{CO}$ | 30.03 | $0.815^{-20}$ | -928.30 | - | -19.3 | 24.48 | - | - | -115.90(g) | $\begin{aligned} & -563.46(\mathrm{~g}) \\ & -262.8(\mathrm{l}) \end{aligned}$ |
| Formic acid | $\mathrm{CH}_{2} \mathrm{O}_{2}$ | 46.03 | 1.220 |  | 12.68 | 100.5 | 22.25 | - | - | -409.2(1) |  |
| Glycerol | $\mathrm{C}_{3} \mathrm{H}_{8} \mathrm{O}_{3}$ | 92.09 | $1.260^{50}$ | 18.20 | 18.30 | 290.0 | - | - | - | $-362.6(\mathrm{~g})$ $-665.9(\mathrm{l})$ | -1661.1(1) |
| Helium | He | 4.00 | - | -269.7 | 0.02 | -268.9 | 0.084 | 5.26 | 2.26 | $0(\mathrm{~g})$ | , |
| $n$-Heptane | $\mathrm{C}_{7} \mathrm{H}_{16}$ | 100.20 | 0.684 | -90.59 | 14.03 | 98.43 | 31.69 | 540.2 | 27.0 | $\begin{aligned} & -224.4(\mathrm{l}) \\ & -187.8(\mathrm{~g}) \end{aligned}$ | $\begin{aligned} & -4816.9(1) \\ & -4853.5(\mathrm{~g}) \end{aligned}$ |
| $n$-Hexane | $\mathrm{C}_{6} \mathrm{H}_{14}$ | 86.17 | 659 | -95.32 | 13.03 | 68.74 | 28.85 | 507.9 | 29.9 | $\begin{aligned} & -198.8(\mathrm{l}) \\ & -167.2(\mathrm{~g}) \end{aligned}$ | $\begin{aligned} & -4163.1(\mathrm{l}) \\ & -4194.8(\mathrm{~g}) \end{aligned}$ |
| Hydrogen | $\mathrm{H}_{2}$ | 2.016 | - | -259.19 | 0.12 | -252.76 | 0.904 | 33.3 | 12.8 | $0(\mathrm{~g})$ $-36.23(\mathrm{~g})$ | $-285.84(\mathrm{~g})$ - |
| Hydrogen | HBr | 80.92 | - | -86 | - | -67 |  |  |  |  |  |
| bromide Hydrogen | HCl | 36.47 |  | -114.2 | 1.99 | -85.0 | 16.1 | 324.6 | 81.5 | -92.31(g) | - |
| Hydrogen chloride | HCl | 36.47 | - | -14 |  |  | - | - | - | +130.54(g) | - |
| Hydrogen cyanide | HCN | 27.03 | - | -14 | - | 26 | - | 503.2 | - | $-268.6(\mathrm{~g})$ |  |
| Hydrogen fluoride | HF | 20.0 | - | -83 | - | 20 | - | 503.2 | - | $\begin{gathered} -268.6(\mathrm{~g}) \\ -316.9(\mathrm{aq}, \\ 200) \end{gathered}$ | - |
|  | $\mathrm{H}_{2} \mathrm{~S}$ | 34.08 | - | -85.5 | 2.38 | -60.3 | 18.67 | 373.6 | 88.9 | -19.96(g) | -562.59(g) |
| sulfide | $\mathrm{H}_{2}$ |  |  |  |  |  | - | 826.0 | - | 0 (c) | - |
| Iodine | $\mathrm{I}_{2}$ | 253.8 55.85 | 4.93 7.7 | $\begin{gathered} 113.3 \\ 1535 \end{gathered}$ | 15.1 | 2800 | 354.0 | 82 | - | 0 (c) | - |
| Iron | Fe Pb | 55.85 207.21 | $1.1337^{720 / 20^{\circ}}$ | 1535 327.4 | 5.10 | 1750 | 179.9 | - |  | O(c) | - |
| Lead oxide | PbO | 223.21 | 9.5 | 886 | 11.7 | 1472 | 213 | - | - | -219.2(c) | - |
| Magnesium | Mg | 24.32 | 1.74 | 650 | 9.2 | 1120 | 131.8 136.8 | - | - | -641.8(c) | - |
| Magnesium chloride | $\mathrm{MgCl}_{2}$ | 95.23 | $2.325^{25^{\circ}}$ | 714 | 43.1 | 1418 | 136.8 | - | - | - |  |
| Magnesium | $\mathrm{Mg}(\mathrm{OH})_{2}$ | 58.34 | 2.4 |  | Decomposes at $350^{\circ} \mathrm{C}$ |  |  | - |  |  |  |  |
| hydroxide |  | 40.32 | 3.65 | 2900 | 77.4 | 3600 | - | - | - | -601.8(c) | - |
| Magnesium oxide | MgO | 40.32 | 3.65 |  |  |  |  |  | - | 0(c) | - |
| Mercury | Hg | 200.61 | 13.546 | -38.87 | $\overline{0.94}$ | -356.9 -161.5 | $\overline{8.179}$ | 190.70 | 45.8 | -74.85(g) | -890.36(g) |
| Methane | $\mathrm{CH}_{4}$ | 16.04 | 33 | -182.5 | 0.94 | - 57.1 |  |  | 46.30 | -409.4(1) | -1595(1) |
| Methyl acetate | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}_{2}$ | 74.08 | 0.933 | -98.9 | - | 57.1 | - | 513.20 | 78.50 | $-238.6(1)$ | 726.6 (1) |
| Methyl alcohol | $\mathrm{CH}_{3} \mathrm{OH}$ | 32.04 | 0.792 | -97.9 | 3.167 | 64.7 | 35.27 | 513.20 | 78.50 | $-201.2(\mathrm{~g})$ | $-764.0(\mathrm{~g})$ |
| (Methanol) |  | 31.06 | $0.699^{-11^{\circ}}$ | -92.7 | - | -6.9 | - | 429.9 | 73.60 | -28.0(g) | -1071.5(1) |
| Methyl amine | $\mathrm{CH}_{5} \mathrm{~N}$ |  |  |  |  |  |  | 416.1 | 65.80 | -81.92(g) | - |
| Methyl chloride | $\mathrm{CH}_{3} \mathrm{Cl}$ | 50.49 | - | -97.9 | - | -24 | - | 416.1 | 65.80 | -81.92(g) |  |

Table B. 1 (Continued)


Table B. 1 (Continued)

| Compound | Formula | Mol. Wt. | $\begin{gathered} \text { SG } \\ \left(20^{\circ} / 4^{\circ}\right) \end{gathered}$ | $T_{\mathrm{m}}\left({ }^{\circ} \mathrm{C}\right)^{b}$ | $\begin{gathered} \Delta \hat{H}_{\mathrm{m}}\left(T_{\mathrm{m}}\right)^{c, j} \\ \mathrm{~kJ} / \mathrm{mol} \end{gathered}$ | $T_{\mathrm{b}}\left({ }^{\circ} \mathrm{C}\right)^{d}$ | $\begin{gathered} \Delta \hat{H}_{\mathrm{v}}\left(T_{\mathrm{b}}\right)^{e, j} \\ \mathrm{kJJ} / \mathrm{mol} \end{gathered}$ | $T_{\mathrm{c}}(\mathrm{K})^{f}$ | $\mathrm{P}_{\mathrm{c}}(\mathrm{atm})^{g}$ | $\left(\Delta \hat{H}_{\mathrm{f}}^{\circ}\right)^{h, j}$ <br> $\mathrm{kJ} / \mathrm{mol}$ | $\left(\Delta \hat{H}_{\mathrm{c}}{ }^{\circ}\right)^{i,}$ <br> $\mathrm{kJ} / \mathrm{mol}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sodium | $\mathrm{Na}_{2} \mathrm{~S}_{2} \mathrm{O}_{3}$ | 158.11 | 1.667 | - | - | - | - | - | - | -1117.1(c) | - |
| thiosulfate |  |  |  |  |  |  |  |  |  |  | - |
| Sulfur (rhombic) | $\mathrm{S}_{8}$ | 256.53 | 2.07 | 113 | 10.04 | 444.6 | 83.7 | - | - | 0 (c) | - |
| Sulfur | $\mathrm{S}_{8}$ | 256.53 | 1.96 | 119 | 14.17 | 444.6 | 83.7 | - | - | +0.30 (c) | - |
| (monoclinic) |  |  |  |  |  |  |  |  |  |  |  |
| Sulfur dioxide | $\mathrm{SO}_{2}$ | 64.07 | - | -75.48 | 7.402 | -10.02 | 24.91 | 430.7 | 77.8 | -296.90(g) | - |
| Sulfur | $\mathrm{SO}_{3}$ | 80.07 | - | 16.84 | 25.48 | 43.3 | 41.80 | 491.4 | 83.8 | -395.18(g) | - |
| trioxide |  |  |  |  |  |  |  |  |  |  |  |
| Sulfuric acid | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | 98.08 | $1.834^{18^{\circ}}$ | 10.35 | 9.87 | Decomp | ses at $340^{\circ} \mathrm{C}$ | - | - | $\begin{aligned} & -811.32(\mathrm{l}) \\ & -907.51(\mathrm{aq}) \end{aligned}$ | - |
| Toluene | $\mathrm{C}_{7} \mathrm{H}_{8}$ | 92.13 | 0.866 | -94.99 | 6.619 | 110.62 | 33.47 | 593.9 | 40.3 | +12.00(1) | -3909.9(1) |
|  |  |  |  |  |  |  |  |  |  | +50.00(g) | -3947.9(g) |
| Water | $\mathrm{H}_{2} \mathrm{O}$ | 18.016 | $1.00^{4^{\circ}}$ | 0.00 | 6.0095 | 100.00 | 40.656 | 647.4 | 218.3 | $-285.84(1)$ | - |
|  |  |  |  |  |  |  |  |  |  | -241.83(g) |  |
| $m$-Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | 106.16 | 0.864 | -47.87 | 11.569 | 139.10 | 36.40 | 619 | 34.6 | $-25.42(1)$ | $\begin{aligned} & -4551.9(1) \\ & -45045(\sigma) \end{aligned}$ |
| $o$-Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | 106.16 | 0.880 | -25.18 | 13.598 | 144.42 | 36.82 | 631.5 | 35.7 | -24.44(1) | -4552.9(1) |
| o-Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ |  |  |  |  |  |  |  |  | +18.99(g) | -4596.3(g) |
| $p$-Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | 106.16 | 0.861 | 13.26 | 17.11 | 138.35 | 36.07 | 618 | 33.9 | -24.43(1) | -4552.91(1) |
| p-Xylene |  |  |  |  |  |  |  |  |  | 17.95 (g) | -4595.2(g) |
| Zinc | Zn | 65.38 | 7.140 | 419.5 | 6.674 | 907 | 114.77 | - | - | 0 (c) | - |


|  | Form 2: $C_{p}\left[\mathrm{~kJ} /\left(\mathrm{mol} \cdot{ }^{\circ} \mathrm{C}\right)\right]$ or $[\mathrm{kJ} /(\mathrm{mol} \cdot \mathrm{K})]=a+b T+c T^{-2}$ |
| ---: | :--- |
| Example: $\left(C_{p}\right)_{\text {acetone }(\mathrm{g})}=0.07196+\left(20.10 \times 10^{-5}\right) T-\left(12.78 \times 10^{-8}\right) T^{2}+\left(34.76 \times 10^{-12}\right) T^{3}$, where $T$ is in ${ }^{\circ} \mathrm{C}$. |  |




From Elementary Principles of Chemical Processes, 3'rd ed.; R.M. Felder and R.W. Rousseau.

Table B. 5 Properties of Saturated Steam: Temperature Table ${ }^{a}$

| $T\left({ }^{\circ} \mathrm{C}\right)$ | $P$ (bar) | $\hat{V}\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ |  | $\hat{U}(\mathrm{~kJ} / \mathrm{kg})$ |  | $\hat{H}(\mathrm{~kJ} / \mathrm{kg})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Water | Steam | Water | Steam | Water | Evaporation | Steam |
| 0.01 | 0.00611 | 0.001000 | 206.2 | zero | 2375.6 | +0.0 | 2501.6 | 2501.6 |
| 2 | 0.00705 | 0.001000 | 179.9 | 8.4 | 2378.3 | 8.4 | 2496.8 | 2505.2 |
| 4 | 0.00813 | 0.001000 | 157.3 | 16.8 | 2381.1 | 16.8 | 2492.1 | 2508.9 |
| 6 | 0.00935 | 0.001000 | 137.8 | 25.2 | 2383.8 | 25.2 | 2487.4 | 2512.6 |
| 8 | 0.01072 | 0.001000 | 121.0 | 33.6 | 2386.6 | 33.6 | 2482.6 | 2516.2 |
| 10 | 0.01227 | 0.001000 | 106.4 | 42.0 | 2389.3 | 42.0 | 2477.9 | 2519.9 |
| 12 | 0.01401 | 0.001000 | 93.8 | 50.4 | 2392.1 | 50.4 | 2473.2 | 2523.6 |
| 14 | 0.01597 | 0.001001 | 82.9 | 58.8 | 2394.8 | 58.8 | 2468.5 | 2527.2 |
| 16 | 0.01817 | 0.001001 | 73.4 | 67.1 | 2397.6 | 67.1 | 2463.8 | 2530.9 |
| 18 | 0.02062 | 0.001001 | 65.1 | 75.5 | 2400.3 | 75.5 | 2459.0 | 2534.5 |
| 20 | 0.0234 | 0.001002 | 57.8 | 83.9 | 2403.0 | 83.9 | 2454.3 | 2538.2 |
| 22 | 0.0264 | 0.001002 | 51.5 | 92.2 | 2405.8 | 92.2 | 2449.6 | 2541.8 |
| 24 | 0.0298 | 0.001003 | 45.9 | 100.6 | 2408.5 | 100.6 | 2444.9 | 2545.5 |
| 25 | 0.0317 | 0.001003 | 43.4 | 104.8 | 2409.9 | 104.8 | 2442.5 | 2547.3 |
| 26 | 0.0336 | 0.001003 | 41.0 | 108.9 | 2411.2 | 108.9 | 2440.2 | 2549.1 |
| 28 | 0.0378 | 0.001004 | 36.7 | 117.3 | 2414.0 | 117.3 | 2435.4 | 2552.7 |
| 30 | 0.0424 | 0.001004 | 32.9 | 125.7 | 2416.7 | 125.7 | 2430.7 | 2556.4 |
| 32 | 0.0475 | 0.001005 | 29.6 | 134.0 | 2419.4 | 134.0 | 2425.9 | 2560.0 |
| 34 | 0.0532 | 0.001006 | 26.6 | 142.4 | 2422.1 | 142.4 | 2421.2 | 2563.6 |
| 36 | 0.0594 | 0.001006 | 24.0 | 150.7 | 2424.8 | 150.7 | 2416.4 | 2567.2 |
| 38 | 0.0662 | 0.001007 | 21.6 | 159.1 | 2427.5 | 159.1 | 2411.7 | 2570.8 |
| 40 | 0.0738 | 0.001008 | 19.55 | 167.4 | 2430.2 | 167.5 | 2406.9 | 2574.4 |
| 42 | 0.0820 | 0.001009 | 17.69 | 175.8 | 2432.9 | 175.8 | 2402.1 | 2577.9 |
| 44 | 0.0910 | 0.001009 | 16.04 | 184.2 | 2435.6 | 184.2 | 2397.3 | 2581.5 |
| 46 | 0.1009 | 0.001010 | 14.56 | 192.5 | 2438.3 | 192.5 | 2392.5 | 2585.1 |
| 48 | 0.1116 | 0.001011 | 13.23 | 200.9 | 2440.9 | 200.9 | 2387.7 | 2588.6 |
| 50 | 0.1234 | 0.001012 | 12.05 | 209.2 | 2443.6 | 209.3 | 2382.9 | 2592.2 |
| 52 | 0.1361 | 0.001013 | 10.98 | 217.7 | 2446 | 217.7 | 2377 | 2595 |
| 54 | 0.1500 | 0.001014 | 10.02 | 226.0 | 2449 | 226.0 | 2373 | 2599 |
| 56 | 0.1651 | 0.001015 | 9.158 | 234.4 | 2451 | 234.4 | 2368 | 2602 |
| 58 | 0.1815 | 0.001016 | 8.380 | 242.8 | 2454 | 242.8 | 2363 | 2606 |
| 60 | 0.1992 | 0.001017 | 7.678 | 251.1 | 2456 | 251.1 | 2358 | 2609 |
| 62 | 0.2184 | 0.001018 | 7.043 | 259.5 | 2459 | 259.5 | 2353 | 2613 |
| 64 | 0.2391 | 0.001019 | 6.468 | 267.9 | 2461 | 267.9 | 2348 | 2616 |
| 66 | 0.2615 | 0.001020 | 5.947 | 276.2 | 2464 | 276.2 | 2343 | 2619 |
| 68 | 0.2856 | 0.001022 | 5.475 | 284.6 | 2467 | 284.6 | 2338 | 2623 |

${ }^{a}$ From R. W. Haywood, Thermodynamic Tables in SI (Metric) Units, Cambridge University Press, London, 1968. $\hat{V}=$ specific volume, $\hat{U}=$ specific internal energy, and $\hat{H}=$ specific enthalpy. Note: $\mathrm{kJ} / \mathrm{kg} \times 0.4303=\mathrm{Btu} / \mathrm{l}_{\mathrm{m}}$.

Table B. 5 (Continued)

| $T\left({ }^{\circ} \mathrm{C}\right)$ | $P($ bar $)$ | $\hat{V}\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ |  | $\hat{U}(\mathrm{~kJ} / \mathrm{kg})$ |  | $\hat{H}(\mathrm{~kJ} / \mathrm{kg})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Water | Steam | Water | Steam | Water | Evaporation | Steam |
| 70 | 0.3117 | 0.001023 | 5.045 | 293.0 | 2469 | 293.0 | 2333 | 2626 |
| 72 | 0.3396 | 0.001024 | 4.655 | 301.4 | 2472 | 301.4 | 2329 | 2630 |
| 74 | 0.3696 | 0.001025 | 4.299 | 309.8 | 2474 | 309.8 | 2323 | 2633 |
| 76 | 0.4019 | 0.001026 | 3.975 | 318.2 | 2476 | 318.2 | 2318 | 2636 |
| 78 | 0.4365 | 0.001028 | 3.679 | 326.4 | 2479 | 326.4 | 2313 | 2639 |
| 80 | 0.4736 | 0.001029 | 3.408 | 334.8 | 2482 | 334.9 | 2308 | 2643 |
| 82 | 0.5133 | 0.001030 | 3.161 | 343.2 | 2484 | 343.3 | 2303 | 2646 |
| 84 | 0.5558 | 0.001032 | 2.934 | 351.6 | 2487 | 351.7 | 2298 | 2650 |
| 86 | 0.6011 | 0.001033 | 2.727 | 360.0 | 2489 | 360.1 | 2293 | 2653 |
| 88 | 0.6495 | 0.001034 | 2.536 | 368.4 | 2491 | 368.5 | 2288 | 2656 |
| 90 | 0.7011 | 0.001036 | 2.361 | 376.9 | 2493 | 377.0 | 2282 | 2659 |
| 92 | 0.7560 | 0.001037 | 2.200 | 385.3 | 2496 | 385.4 | 2277 | 2662 |
| 94 | 0.8145 | 0.001039 | 2.052 | 393.7 | 2499 | 393.8 | 2272 | 2666 |
| 96 | 0.8767 | 0.001040 | 1.915 | 402.1 | 2501 | 402.2 | 2267 | 2669 |
| 98 | 0.9429 | 0.001042 | 1.789 | 410.6 | 2504 | 410.7 | 2262 | 2673 |
| 100 | 1.0131 | 0.001044 | 1.673 | 419.0 | 2507 | 419.1 | 2257 | 2676 |
| 102 | 1.0876 | 0.001045 | 1.566 | 427.1 | 2509 | 427.5 | 2251 | 2679 |

Table B. 6 Properties of Saturated Steam: Pressure Tablea

| $P$ (bar) | $T\left({ }^{\circ} \mathrm{C}\right)$ | $\hat{V}\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ |  | $\hat{O}(\mathrm{~kJ} / \mathrm{kg})$ |  | $\hat{H}(\mathrm{~kJ} / \mathrm{kg})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Water | Steam | Water | Steam | Water | Evaporation | Steam |
| 0.00611 | 0.01 | 0.001000 | 206.2 | zero | 2375.6 | +0.0 | 2501.6 | 2501.6 |
| 0.008 | 3.8 | 0.001000 | 159.7 | 15.8 | 2380.7 | 15.8 | 2492.6 | 2508.5 |
| 0.010 | 7.0 | 0.001000 | 129.2 | 29.3 | 2385.2 | 29.3 | 2485.0 | 2514.4 |
| 0.012 | 9.7 | 0.001000 | 108.7 | 40.6 | 2388.9 | 40.6 | 2478.7 | 2519.3 |
| 0.014 | 12.0 | 0.001000 | 93.9 | 50.3 | 2392.0 | 50.3 | 2473.2 | 2523.5 |
| 0.016 | 14.0 | 0.001001 | 82.8 | 58.9 | 2394.8 | 58.9 | 2468.4 | 2527.3 |
| 0.018 | 15.9 | 0.001001 | 74.0 | 66.5 | 2397.4 | 66.5 | 2464.1 | 2530.6 |
| 0.020 | 17.5 | 0.001001 | 67.0 | 73.5 | 2399.6 | 73.5 | 2460.2 | 2533.6 |
| 0.022 | 19.0 | 0.001002 | 61.2 | 79.8 | 2401.7 | 79.8 | 2456.6 | 2536.4 |
| 0.024 | 20.4 | 0.001002 | 56.4 | 85.7 | 2403.6 | 85.7 | 2453.3 | 2539.0 |
| 0.026 | 21.7 | 0.001002 | 52.3 | 91.1 | 2405.4 | 91.1 | 2450.2 | 2541.3 |
| 0.028 | 23.0 | 0.001002 | 48.7 | 96.2 | 2407.1 | 96.2 | 2447.3 | 2543.6 |
| 0.030 | 24.1 | 0.001003 | 45.7 | 101.0 | 2408.6 | 101.0 | 2444.6 | 2545.6 |
| 0.035 | 26.7 | 0.001003 | 39.5 | 111.8 | 2412.2 | 111.8 | 2438.5 | 2550.4 |
| 0.040 | 29.0 | 0.001004 | 34.8 | 121.4 | 2415.3 | 121.4 | 2433.1 | 2554.5 |
| 0.045 | 31.0 | 0.001005 | 31.1 | 130.0 | 2418.1 | 130.0 | 2428.2 | 2558.2 |
| 0.050 | 32.9 | 0.001005 | 28.2 | 137.8 | 2420.6 | 137.8 | 2423.8 | 2561.6 |
| 0.060 | 36.2 | 0.001006 | 23.74 | 151.5 | 2425.1 | 151.5 | 2416.0 | 2567.5 |
| 0.070 | 39.0 | 0.001007 | 20.53 | 163.4 | 2428.9 | 163.4 | 2409.2 | 2572.6 |
| 0.080 | 41.5 | 0.001008 | 18.10 | 173.9 | 2432.3 | 173.9 | 2403.2 | 2577.1 |
| 0.090 | 43.8 | 0.001009 | 16.20 | 183.3 | 2435.3 | 183.3 | 2397.9 | 2581.1 |
| 0.10 | 45.8 | 0.001010 | 14.67 | 191.8 | 2438.0 | 191.8 | 2392.9 | 2584.8 |
| 0.11 | 47.7 | 0.001011 | 13.42 | 199.7 | 2440.5 | 199.7 | 2388.4 | 2588.1 |
| 0.12 | 49.4 | 0.001012 | 12.36 | 206.9 | 2442.8 | 206.9 | 2384.3 | 2591.2 |
| 0.13 | 51.1 | 0.001013 | 11.47 | 213.7 | 2445.0 | 213.7 | 2380.4 | 2594.0 |
| 0.14 | 52.6 | 0.001013 | 10.69 | 220.0 | 2447.0 | 220.0 | 2376.7 | 2596.7 |
| 0.15 | 54.0 | 0.001014 | 10.02 | 226.0 | 2448.9 | 226.0 | 2373.2 | 2599.2 |
| 0.16 | 55.3 | 0.001015 | 9.43 | 231.6 | 2450.6 | 231.6 | 2370.0 | 2601.6 |
| 0.17 | 56.6 | 0.001015 | 8.91 | 236.9 | 2452.3 | 236.9 | 2366.9 | 2603.8 |
| 0.18 | 57.8 | 0.001016 | 8.45 | 242.0 | 2453.9 | 242.0 | 2363.9 | 2605.9 |
| 0.19 | 59.0 | 0.001017 | 8.03 | 246.8 | 2455.4 | 246.8 | 2361.1 | 2607.9 |
| 0.20 | 60.1 | 0.001017 | 7.65 | 251.5 |  |  |  |  |
| 0.22 | 62.2 | 0.001018 | 7.00 | 260.1 | 2459.6 | 260.1 | 23553.3 | 2609.9 2613.5 |
| 0.24 | 64.1 | 0.001019 | 6.45 | 268.2 | 2462.1 | 268.2 | 2348.6 | 2616.8 |
| 0.26 | 65.9 | 0.001020 | 5.98 | 275.6 | 2464.4 | 275.7 | 2344.2 | 2619.9 |
| 0.28 | 67.5 | 0.001021 | 5.58 | 282.7 | 2466.5 | 282.7 | 2340.0 | 2622.7 |
| 0.30 | 69.1 | 0.001022 | 5.23 | 289.3 | 2468.6 | 289.3 | 2336.1 | 2625.4 |
| 0.35 | 72.7 | 0.001025 | 4.53 | 304.3 | 2473.1 | 304.3 | 2327.2 | 2631.5 |
| 0.40 | 75.9 | 0.001027 | 3.99 | 317.6 | 2477.1 | 317.7 | 2319.2 | 2636.9 |
| 0.45 | 78.7 | 0.001028 | 3.58 | 329.6 | 2480.7 | 329.6 | 2312.0 | 2641.7 |
| 0.50 | 81.3 | 0.001030 | 3.24 | 340.5 | 2484.0 | 340.6 | 2305.4 | 2646.0 |
| 0.55 0.60 | 83.7 86.0 | 0.001032 | 2.96 | 350.6 | 2486.9 | 350.6 | 2299.3 | 2649.9 |
| 0.60 | 86.0 | 0.001033 | 2.73 | 359.9 | 2489.7 | 359.9 | 2293.6 | 2653.6 |
| 0.65 | 88.0 | 0.001035 | 2.53 | 368.5 | 2492.2 | 368.6 | 2288.3 | 2656.9 |
| 0.70 | 90.0 | 0.001036 | 2.36 | 376.7 | $249+5$ | 376.8 | 2283.3 | 2660.1 |
| 0.75 | 91.8 | 0.001037 | 2.22 | 384.4 | 2496.7 | 384.5 | 2278.6 | 2663.0 |
| 0.80 | 93.5 | 0.001039 | 2.087 | 391.6 | 2498.8 | 391.7 | 2274.1 | 2665.8 |
| 0.85 | 95.2 | 0.001040 | 1.972 | 398.5 | 2500.8 | 398.6 | 2269.8 | 2668.4 |
| 0.90 | 96.7 | 0.001041 | 1.869 | 405.1 | 2502.6 | 405.2 | 2265.6 | 2670.9 |
| 0.95 1.00 | 98.2 99.6 | 0.001042 0.001043 | 1.777 1.694 | 411.4 | 2504.4 | 411.5 | 2261.7 | 2673.2 |
| 1.00 1.01325 | 99.6 100.0 | 0.001043 0.001044 | 1.694 1.673 | 417.4 419.0 | 2506.1 2506.5 | 417.5 | 2257.9 | 2675.4 |
| (1 1 atm ) | 10.0 | 0.001044 | 1.673 | 419.0 | 2506.5 | 419.1 | 2256.9 | 2676.0 |

${ }^{a}$ From R. W. Haywood, Thermodynamic Tables in SI (Metric) Units, Cambridge University Press, London, 1968. $\hat{v}=$ specific volume, $\hat{U}=$ specific internal energy, and $\hat{H}=$ specific enthalpy. Note: $\mathrm{kJ} / \mathrm{kg} \times 0.4303=\mathrm{Btu} / \mathrm{lb}_{\mathrm{m}}$.

Table B. 6 (Continued)

| $P($ bar $)$ | $T\left({ }^{\circ} \mathrm{C}\right)$ | $\hat{V}\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ |  | $\hat{U}(\mathrm{~kJ} / \mathrm{kg})$ |  | $\hat{H}(\mathrm{~kJ} / \mathrm{kg})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Water | Steam | Water | Steam | Water | Evaporation | Steam |
| 1.1 | 102.3 | 0.001046 | 1.549 | 428.7 | 2509.2 | 428.8 | 2250.8 | 2679.6 |
| 1.2 | 104.8 | 0.001048 | 1.428 | 439.2 | 2512.1 | 439.4 | 2244.1 | 2683.4 |
| 1.3 | 107.1 | 0.001049 | 1.325 | 449.1 | 2514.7 | 449.2 | 2237.8 | 2687.0 |
| 1.4 | 109.3 | 0.001051 | 1.236 | 458.3 | 2517.2 | 458.4 | 2231.9 | 2690.3 |
| 1.5 | 111.4 | 0.001053 | 1.159 | 467.0 | 2519.5 | 467.1 | 2226.2 | 2693.4 |
| 1.6 | 113.3 | 0.001055 | 1.091 | 475.2 | 2521.7 | 475.4 | 2220.9 | 2696.2 |
| 1.7 | 115.2 | 0.001056 | 1.031 | 483.0 | 2523.7 | 483.2 | 2215.7 | 2699.0 |
| 1.8 | 116.9 | 0.001058 | 0.977 | 490.5 | 2525.6 | 490.7 | 2210.8 | 2701.5 |
| 1.9 | 118.6 | 0.001059 | 0.929 | 497.6 | 2527.5 | 497.8 | 2206.1 | 2704.0 |
| 2.0 | 120.2 | 0.001061 | 0.885 | 504.5 | 2529.2 | 504.7 | 2201.6 | 2706.3 |
| 2.2 | 123.3 | 0.001064 | 0.810 | 517.4 | 2532.4 | 517.6 | 2193.0 | 2710.6 |
| 2.4 | 126.1 | 0.001066 | 0.746 | 529.4 | 2535.4 | 529.6 | 2184.9 | 2714.5 |
| 2.6 | 128.7 | 0.001069 | 0.693 | 540.6 | 2538.1 | 540.9 | 2177.3 | 2718.2 |
| 2.8 | 131.2 | 0.001071 | 0.646 | 551.1 | 2540.6 | 551.4 | 2170.1 | 2721.5 |
| 3.0 | 133.5 | 0.001074 | 0.606 | 561.1 | 2543.0 | 561.4 | 2163.2 | 2724.7 |
| 3.2 | 135.8 | 0.001076 | 0.570 | 570.6 | 2545.2 | 570.9 | 2156.7 | 2727.6 |
| 3.4 | 137.9 | 0.001078 | 0.538 | 579.6 | 2547.2 | 579.9 | 2150.4 | 2730.3 |
| 3.6 | 139.9 | 0.001080 | 0.510 | 588.1 | 2549.2 | 588.5 | 2144.4 | 2732.9 |
| 3.8 | 141.8 | 0.001082 | 0.485 | 596.4 | 2551.0 | 596.8 | 2138.6 | 2735.3 |
| 4.0 | 143.6 | 0.001084 | 0.462 | 604.2 | 2552.7 | 604.7 | 2133.0 | 2737.6 |
| 4.2 | 145.4 | 0.001086 | 0.442 | 611.8 | 2554.4 | 612.3 | 2127.5 | 2739.8 |
| 4.4 | 147.1 | 0.001088 | 0.423 | 619.1 | 2555.9 | 619.6 | 2122.3 | 2741.9 |
| 4.6 | 148.7 | 0.001089 | 0.405 | 626.2 | 2557.4 | 626.7 | 2117.2 | 2743.9 |
| 4.8 | 150.3 | 0.001091 | 0.389 | 633.0 | 2558.8 | 633.5 | 2112.2 | 2745.7 |
| 5.0 | 151.8 | 0.001093 | 0.375 | 639.6 | 2560.2 | 640.1 | 2107.4 | 2747.5 |
| 5.5 | 155.5 | 0.001097 | 0.342 | 655.2 | 2563.3 | 655.8 | 2095.9 | 2751.7 |
| 6.0 | 158.8 | 0.001101 | 0.315 | 669.8 | 2566.2 | 670.4 | 2085.0 | 2755.5 |
| 6.5 | 162.0 | 0.001105 | 0.292 | 683.4 | 2568.7 | 684.1 | 2074.7 | 2758.9 |
| 7.0 | 165.0 | 0.001108 | 0.273 | 696.3 | 2571.1 | 697.1 | 2064.9 | 2762.0 |
| 7.5 | 167.8 | 0.001112 | 0.2554 | 708.5 | 2573.3 | 709.3 | 2055.5 | 2764.8 |
| 8.0 | 170.4 | 0.001115 | 0.2403 | 720.0 | 2575.5 | 720.9 | 2046.5 | 2767.5 |
| 8.5 | 172.9 | 0.001118 | 0.2268 | 731.1 | 2577.1 | 732.0 | 2037.9 | 2769.9 |
| 9.0 | 175.4 | 0.001121 | 0.2148 | 741.6 | 2578.8 | 742.6 | 2029.5 | 2772.1 |
| 9.5 | 177.7 | 0.001124 | 0.2040 | 751.8 | 2580.4 | 752.8 | 2021.4 | 2774.2 |
| 10.0 | 179.9 | 0.001127 | 0.1943 | 761.5 | 2581.9 | 762.6 | 2013.6 | 2776.2 |
| 10.5 | 182.0 | 0.001130 | 0.1855 | 770.8 | 2583.3 | 772.0 | 2005.9 | 2778.0 |
| 11.0 | 184.1 | 0.001133 | 0.1774 | 779.9 | 2584.5 | 781.1 | 1998.5 | 2779.7 |
| 11.5 | 186.0 | 0.001136 | 0.1700 | 788.6 | 2585.8 | 789.9 | 1991.3 | 2781.3 |
| 12.0 | 188.0 | 0.001139 | 0.1632 | 797.1 | 2586.9 | 798.4 | 1984.3 | 2782.7 |
| 12.5 | 189.8 | 0.001141 | 0.1569 | 805.3 | 2588.0 | 806.7 | 1977.4 | 2784.1 |
| 13.0 | 191.6 | 0.001144 | 0.1511 | 813.2 | 2589.0 | 814.7 | 1970.7 | 2785.4 |
| 14 | 195.0 | 0.001149 | 0.1407 | 828.5 | 2590.8 | 830.1 | 1957.7 | 2787.8 |
| 15 | 198.3 | 0.001154 | 0.1317 | 842.9 | 2592.4 | 844.7 | 1945.2 | 2789.9 |
| 16 | 201.4 | 0.001159 | 0.1237 | 856.7 | 2593.8 | 858.6 | 1933.2 | 2791.7 |
| 17 | 204.3 | 0.001163 | 0.1166 | 869.9 | 2595.1 | 871.8 | 1921.5 | 2793.4 |
| 18 | 207.1 | 0.001168 | 0.1103 | 882.5 | 2596.3 | 884.6 | 1910.3 | 2794.8 |
| 19 | 209.8 | 0.001172 | 0.1047 | 894.6 | 2597.3 | 896.8 | 1899.3 | 2796.1 |
| 20 | 212.4 | 0.001177 | 0.0995 | 906.2 | 2598.2 | 908.6 | 1888.6 | 2797.2 |
| 21 | 214.9 | 0.001181 | 0.0949 | 917.5 | 2598.9 | 920.0 | 1878.2 | 2798.2 |
| 22 | 217.2 | 0.001185 | 0.0907 | 928.3 | 2599.6 | 931.0 | 1868.1 | 2799.1 |
| 23 | 219.6 | 0.001189 | 0.0868 | 938.9 | 2600.2 | 941.6 | 1858.2 | 2799.8 |
| 24 | 221.8 | 0.001193 | 0.0832 | 949.1 | 2600.7 | 951.9 | 1848.5 | 2800.4 |
| 25 | 223.9 | 0.001197 | 0.0799 | 959.0 | 2601.2 | 962.0 | 1839.0 | 2800.9 |
| 26 | 226.0 | 0.001201 | 0.0769 | 968.6 | 2601.5 | 971.7 | 1829.6 | 2801.4 |
| 27 | 228.1 | 0.001205 | 0.0740 | 978.0 | 2601.8 | 981.2 | 1820.5 | 2801.7 |
| 28 | 230.0 | 0.001209 | 0.0714 | 987.1 | 2602.1 | 990.5 | 1811.5 | 2802.0 |
| 29 | 232.0 | 0.001213 | 0.0689 | 996.0 | 2602.3 | 999.5 | 1802.6 | 2802.2 |
| 30 | 233.8 | 0.001216 | 0.0666 | 1004.7 | 2602.4 | 1008.4 | 1793.9 | 2802.3 |
| 32 | 237.4 | 0.001224 | 0.0624 | 1021.5 | 2602.5 | 1025.4 | 1776.9 | 2802.3 |
| 34 | 240.9 | 0.001231 | 0.0587 | 1037.6 | 2602.5 | 1041.8 | 1760.3 | 2802.1 |
| 36 | 244.2 | 0.001238 | 0.0554 | 1053.1 | 2602.2 | 1057.6 | 1744.2 | 2801.7 |
| 38 | 247.3 | 0.001245 | 0.0524 | 1068.0 | 2601.9 | 1072.7 | 1728.4 | 2801.1 |

Table B. 6 (Continued)

| $P$ (bar) | $T\left({ }^{\circ} \mathrm{C}\right)$ | $\hat{V}\left(\mathrm{~m}^{3} / \mathrm{kg}\right)$ |  | $\hat{U}(\mathrm{~kJ} / \mathrm{kg})$ |  | $\hat{H}(\mathrm{~kJ} / \mathrm{kg})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Water | Steam | Water | Steam | Water | Evaporation | Steam |
| 40 | 250.3 | (0.001252 | 0.0497 | 1082.4 | 2601.3 | 1087.4 | 1712.9 | 2800.3 |
| 42 | 253.2 | ().0012.59 | 0.0473 | 1096.3 | 20000.7 | 11101.6 | 1697.8 | 2799.4 |
| 44 | 256.0 | (0.001266 | 0.0451 | 1109.8 | 2599.9 | 1115.4 | 1682.9 | 2798.3 |
| 46 | 258.8 | 0.001272 | 0.0430 | 1122.9 | 2599.1 | 1128.8 | 1668.3 | 2797.1 |
| 48 | 261.4 | 0.001279 | 0.0412 | 1135.6 | 2598.1 | 1141.8 | 1653.9 | 2795.7 |
| 50 | 263.9 | 0.001286 | 0.0394 | 1148.0 | 2597.0 | 1154.5 | 1639.7 | 2794.2 |
| 52 | 266.4 | 0.001292 | 0.0378 | 1160.1 | 2595.9 | 1166.8 | 1625.7 | 2792.6 |
| 54 | 268.8 | 0.001299 | 0.0363 | 1171.9 | 2594.6 | 1178.9 | 1611.9 | 2790.8 |
| 56 | 271.1 | 0.001306 | 0.0349 | 1183.5 | 2593.3 | 1190.8 | 1598.2 | 2789.0 |
| 58 | 273.3 | 0.001312 | 0.0337 | 1194.7 | 2591.9 | 1202.3 | 1584.7 | 2787.0 |
| 60 | 275.6 | 0.001319 | 0.0324 | 1205.8 | 2590.4 | 1213.7 | 1571.3 | 2785.0 |
| 62 | 277.7 | 0.001325 | 0.0313 | 1216.6 | 2588.8 | 1224.8 | 1558.0 | 2782.9 |
| 64 | 279.8 | 0.001332 | 0.0302 | 1227.2 | 2587.2 | 1235.7 | 1544.9 | 2780.6 |
| 66 | 281.8 | 0.001338 | 0.0292 | 1237.6 | 2585.5 | 1246.5 | 1531.9 | 2778.3 |
| 68 | 283.8 | 0.001345 | 0.0283 | 1247.9 | 2583.7 | 1257.0 | 1518.9 | 2775.9 |
| 70 | 285.8 | 0.001351 | 0.0274 | 1258.0 | 2581.8 | 1267.4 | 1506.0 | 2773.5 |
| 72 | 287.7 | 0.001358 | 0.0265 | 1267.9 | 2579.9 | 1277.6 | 1493.3 | 2770.9 |
| 74 | 289.6 | 0.001364 | 0.0257 | 1277.6 | 2578.0 | 1287.7 | 1480.5 | 2768.3 |
| 76 | 291.4 | 0.001371 | 0.0249 | 1287.2 | 2575.9 | 1297.6 | 1467.9 | 2765.5 |
| 78 | 293.2 | 0.001378 | 0.0242 | 1296.7 | 2573.8 | 1307.4 | 1455.3 | 2762.8 |
| 80 | 295.0 | 0.001384 | 0.0235 | 1306.0 | 2571.7 | 1317.1 | 1442.8 | 2759.9 |
| 82 | 296.7 | 0.001391 | 0.0229 | 1315.2 | 2569.5 | 1326.6 | 1430.3 | 2757.0 |
| 84 | 298.4 | 0.001398 | 0.0222 | 1324.3 | 2567.2 | 1336.1 | 1417.9 | 2754.0 |
| 86 | 300.1 | 0.001404 | 0.0216 | 1333.3 | 2564.9 | 1345.4 | 1405.5 | 2750.9 |
| 88 | 301.7 | 0.001411 | 0.0210 | 1342.2 | 2562.6 | 1354.6 | 1393.2 | 2747.8 |
| 90 | 303.3 | 0.001418 | 0.02050 | 1351.0 | 2560.1 | 1363.7 | 1380.9 | 2744.6 |
| 92 | 304.9 | 0.001425 | 0.01996 | 1359.7 | 2557.7 | 1372.8 | 1368.6 | 2741.4 |
| 94 | 306.4 | 0.001432 | 0.01945 | 1368.2 | 2555.2 | 1381.7 | 1356.3 | 2738.0 |
| 96 | 308.0 | 0.001439 | 0.01897 | 1376.7 | 2552.6 | 1390.6 | 1344.1 | 2734.7 |
| 98 | 309.5 | 0.001446 | 0.01849 | 1385.2 | 2550.0 | 1399.3 | 1331.9 | 2731.2 |
| 100 | 311.0 | 0.001453 | 0.01804 | 1393.5 | 2547.3 | 1408.0 | 1319.7 | 2727.7 |
| 105 | 314.6 | 0.001470 | 0.01698 | 1414.1 | 2540.4 | 1429.5 | 1289.2 | 2718.7 |
| 110 | 318.0 | 0.001489 | 0.01601 | 1434.2 | 2533.2 | 1450.6 | 1258.7 | 2709.3 |
| 115 | 321.4 | 0.001507 | 0.01511 | 1454.0 | 2525.7 | 1471.3 | 1228.2 | 2699.5 |
| 120 | 324.6 | 0.001527 | 0.01428 | 1473.4 | 2517.8 | 1491.8 | 1197.4 | 2689.2 |
| 125 | 327.8 | 0.001547 | 0.01351 | 1492.7 | 2509.4 | 1512.0 | 1166.4 | 2678.4 |
| 130 | 330.8 | 0.001567 | 0.01280 | 1511.6 | 2500.6 | 1532.0 | 1135.0 | 2667.0 |
| 135 | 333.8 | 0.001588 | 0.01213 | 1530.4 | 2491.3 | 1551.9 | 1103.1 | 2655.0 |
| 140 | 336.6 | 0.001611 | 0.01150 | 1549.1 | 2481.4 | 1571.6 | 1070.7 | 2642.4 |
| 145 | 339.4 | 0.001634 | 0.01090 | 1567.5 | 2471.0 | 1591.3 | 11037.7 | 2629.1 |
| 150 | 342.1 | 0.001658 | $0.01(1) 34$ | 1586.1 | 2459.9 | 1611.0 | 1004.0 | 2615.0 |
| 155 | 344.8 | 0.001683 | 0.00981 | 1604.6 | 2448.2 | 1630.7 | 969.6 | 2600.3 |
| 160 | 347.3 | 0.001710 | 0.00931 | 1623.2 | 2436.0 | 1650.5 | 934.3 | 2584.9 |
| 165 | 349.8 | 0.001739 | 0.00883 | 1641.8 | 2423.1 | 1670.5 | 898.3 | 2568.8 |
| 170 | 352.3 | 0.001770 | 0.00837 | 1661.6 | 2409.3 | 1691.7 | 859.9 | 2551.6 |
| 175 | 354.6 | 0.001803 | 0.00793 | 1681.8 | 2394.6 | 1713.3 | 820.0 | 2533.3 |
| 180 | 357.0 | 0.001840 | 0.00750 | 1701.7 | 2378.9 | 1734.8 | 779.1 | 2513.9 |
| 185 | 359.2 | 0.001881 | 0.00708 | 1721.7 | 2362.1 | 1756.5 | 736.6 | 2493.1 |
| 190 | 361.4 | 0.001926 | 0.00668 | 1742.1 | 2343.8 | 1778.7 | 692.0 | 2470.6 |
| 195 | 363.6 | 0.001977 | 0.00628 | 1763.2 | 2323.6 | 1801.8 | 644.2 | 2446.0 |
| 200 | 365.7 | (0).00204 | 0.00588 | 1785.7 | 2300.8 | 1826.5 | 591.9 | 2418.4 |
| 205 | 367.8 | 0.00211 | 0.00546 | 1810.7 | 2274.4 | 1853.9 | 532.5 | 2386.4 |
| 210 | 369.8 | 0.00220 | 0.00502 | 1840.0 | 2242.1 | 1886.3 | 461.3 | 2347.6 |
| 215 | 371.8 | 0.00234 | 0.00451 | 1878.6 | 2198.1 | 1928.9 | 366.2 | 2295.2 |
| 220 | 373.7 | 0.00267 | 0.00373 | 1952 | 2114 | 2011 | 185 | 2196 |
| 221.2 | 374.15 | 0.00317 | 0.00317 | 2038 | 2038 | 2108 | 0 | 2108 |
| (Critical point) |  |  |  |  |  |  |  |  |

Table B. 8 Specific Enthalpies of Selected Gases: SI Units

$$
\hat{H}(\mathrm{~kJ} / \mathrm{mol})
$$

Reference state: Gas, $P_{\text {ref }}=1 \mathrm{~atm}, T_{\text {ref }}=25^{\circ} \mathrm{C}$

| $T$ | Air | $\mathrm{O}_{2}$ | $\mathrm{~N}_{2}$ | $\mathrm{H}_{2}$ | CO | $\mathrm{CO}_{2}$ | $\mathrm{H}_{2} \mathrm{O}$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{0}$ | -0.72 | -0.73 | -0.73 | -0.72 | -0.73 | -0.92 | -0.84 |
| $\mathbf{2 5}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| $\mathbf{1 0 0}$ | 2.19 | 2.24 | 2.19 | 2.16 | 2.19 | 2.90 | 2.54 |
| $\mathbf{2 0 0}$ | 5.15 | 5.31 | 5.13 | 5.06 | 5.16 | 7.08 | 6.01 |
| $\mathbf{3 0 0}$ | 8.17 | 8.47 | 8.12 | 7.96 | 8.17 | 11.58 | 9.57 |
| $\mathbf{4 0 0}$ | 11.24 | 11.72 | 11.15 | 10.89 | 11.25 | 16.35 | 13.23 |
| $\mathbf{5 0 0}$ | 14.37 | 15.03 | 14.24 | 13.83 | 14.38 | 21.34 | 17.01 |
| $\mathbf{6 0 0}$ | 17.55 | 18.41 | 17.39 | 16.81 | 17.57 | 26.53 | 20.91 |
| $\mathbf{7 0 0}$ | 20.80 | 21.86 | 20.59 | 19.81 | 20.82 | 31.88 | 24.92 |
| $\mathbf{8 0 0}$ | 24.10 | 25.35 | 23.86 | 22.85 | 24.13 | 37.36 | 29.05 |
| $\mathbf{9 0 0}$ | 27.46 | 28.89 | 27.19 | 25.93 | 27.49 | 42.94 | 33.32 |
| $\mathbf{1 0 0 0}$ | 30.86 | 32.47 | 30.56 | 29.04 | 30.91 | 48.60 | 37.69 |
| $\mathbf{1 1 0 0}$ | 34.31 | 36.07 | 33.99 | 32.19 | 34.37 | 54.33 | 42.18 |
| $\mathbf{1 2 0 0}$ | 37.81 | 39.70 | 37.46 | 35.39 | 37.87 | 60.14 | 46.78 |
| $\mathbf{1 3 0 0}$ | 41.34 | 43.38 | 40.97 | 38.62 | 41.40 | 65.98 | 51.47 |
| $\mathbf{1 4 0 0}$ | 44.89 | 47.07 | 44.51 | 41.90 | 44.95 | 71.89 | 56.25 |
| $\mathbf{1 5 0 0}$ | 48.45 | 50.77 | 48.06 | 45.22 | 48.51 | 77.84 | 61.09 |

Table B. 9 Specific Enthalpies of Selected Gases:
American Engineering Units

| $\hat{H}(\mathrm{Btu} / \mathrm{lb}-\mathrm{mole})$ <br> Reference state: Gas, $P_{\text {ref }}=1 \mathrm{~atm}, T_{\text {ref }}=77^{\circ} \mathrm{F}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $T$ | Air | $\mathrm{O}_{2}$ | $\mathrm{N}_{2}$ | $\mathrm{H}_{2}$ | CO | $\mathrm{CO}_{2}$ | $\mathrm{H}_{2} \mathrm{O}$ |
| 32 | -312 | -315 | -312 | -310 | -312 | -394 | -361 |
| 77 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 100 | 160 | 162 | 160 | 159 | 160 | 206 | 6 |
| 200 | 858 | 875 | 857 | 848 | 859 | 1132 | 996 |
| 300 | 1563 | 1602 | 1558 | 1539 | 1564 | 2108 | 1818 |
| 400 | 2275 | 2342 | 2265 | 2231 | 2276 | 3129 | 2652 |
| 500 | 2993 | 3094 | 2976 | 2925 | 2994 | 4192 | 3499 4359 |
| 600 | 3719 | 3858 | 3694 | 3621 | 3720 | 6429 | 4359 |
| 700 | 4451 | 4633 | 4418 | 4319 | 4454 | 6429 | 5233 |
| 800 | 5192 | 5418 | 5150 | 5021 | 5195 | 7599 | 6122 |
| 900 | 5940 | 6212 | 5889 | 5725 | 5945 | 8790 | 7025 |
| 1000 | 6695 | 7015 | 6635 | 6433 | 6702 | 10015 | 7944 |
| 1100 | 7459 | 7826 | 7399 | 7145 | 7467 | 11263 | 8880 |
| 1200 | 8230 | 8645 | 8151 | 7861 | 8239 | 12533 | 9831 |
| 1300 | 9010 | 9471 | 8922 | 8581 | 9021 | 13820 | 10799 |
| 1400 | 9797 | 10304 | 9699 | 9306 | 9809 | 15122 | 11783 |
| 1500 | 10590 | 11142 | 10485 | 10035 | 10606 | 16436 | 12783 |
| 1600 | 11392 | 11988 | 11278 | 10769 | 11409 | 17773 | 137981 |
| 1700 | 12200 | 12836 | 12080 | 11509 | 12220 | 19119 | 14831 |
| 1800 | 13016 | 13691 | 12888 | 12254 | 13036 13858 | 20469 | 16941 |
| 1900 | 13837 | 14551 | 13702 14524 | 13003 13759 | 13858 14688 | 23211 | 18019 |
| 2000 | 14663 | 15415 | 14524 | 13759 | 14680 |  |  |

